

LABORATORY OF CYBER-PHYSICAL SYSTEMS

Skoltech

Skolkovo Institute of Science and Technology



▣ Data Science

▣ Space Systems

▣ Biotechnology

▣ Petroleum Engineering

▣ Photonics and Quantum
Materials

▣ Advanced Manufacturing
and Materials

▣ Mathematical Physics

▣ Materials Science

▣ Computational Science
and Engineering



AGENDA

- About Skoltech Cyber-Physical Laboratory
- Project-oriented courses in Skoltech
- pSeven in industrial applications
- pSeven in educational applications
- pSeven in scientific – industrial applications

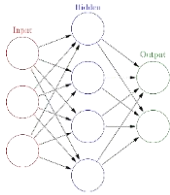


Digital twins
of complex
technical
systems

Industrial AI for
Design
&
Manufacturing

Prescriptive
analytics and
preventive
maintenance

DIGITAL TWIN



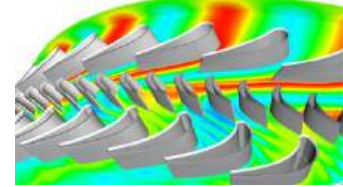
ML* models

- High speed
- Lack of data
- Non-physical models



Physics-based models

- Low speed
- Physics-based



Use data to find the dependencies

- Decision trees
- Random forest
- Neural networks
- Kriging, etc.

Use dependencies to generate data

Numerical methods

- Structural mechanics
- Fluid dynamics
- Heat and mass transfer
- System dynamics

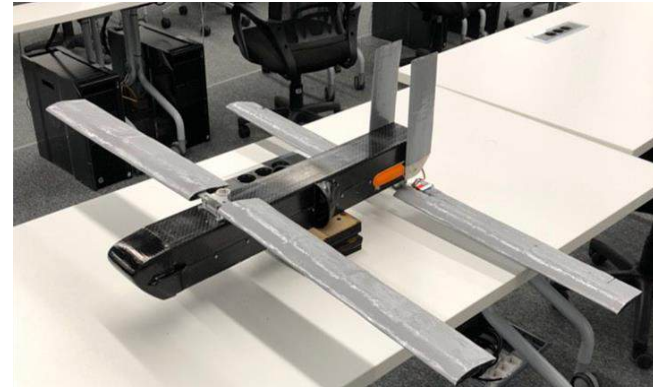
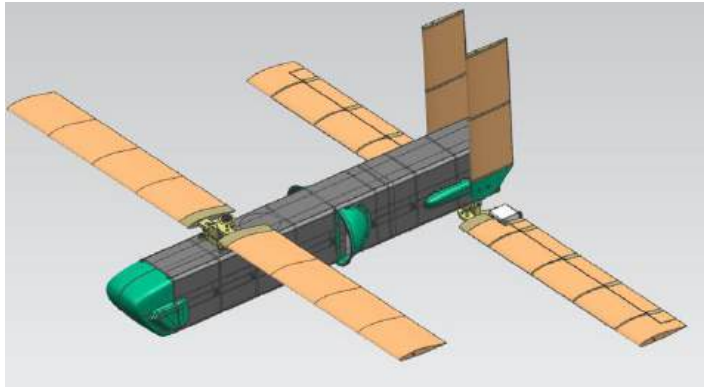
*machine learning

TECHNOLOGY STACK



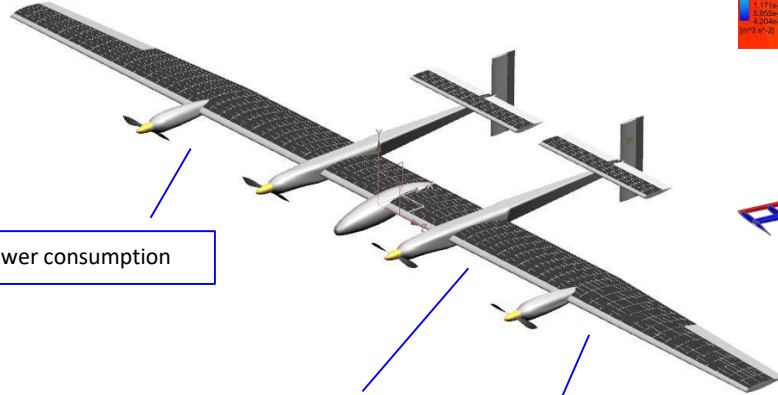
EDUCATION BASED ON PROJECT ORIENTED COURSES

TUBE-LAUNCHED UAV DESIGN AND PROTOTYPE



PROJECT-BASED EDUCATION ON DIGITAL DESIGN. HAPS DESIGN

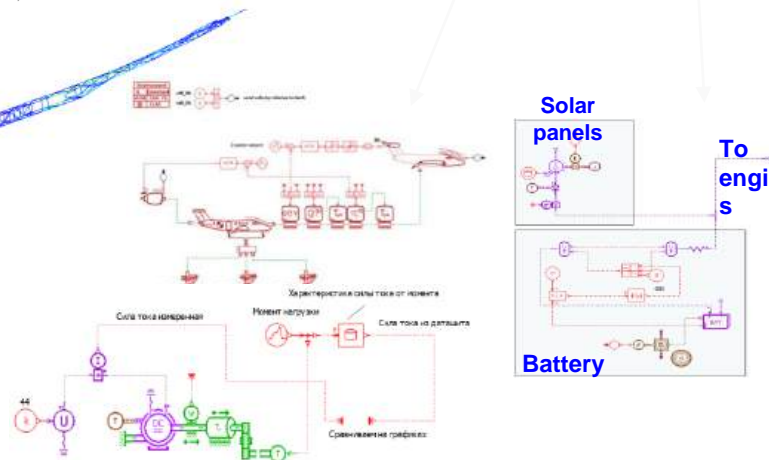
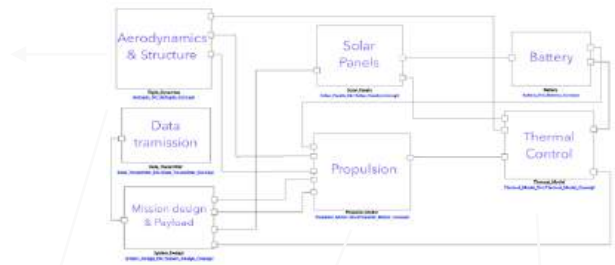
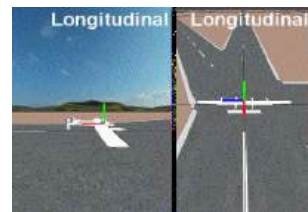
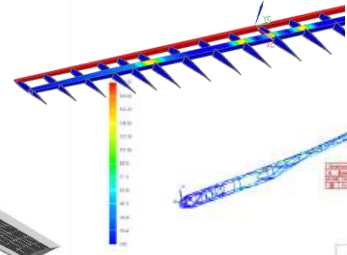
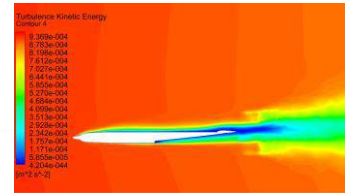
High-Altitude Pseudo Satellite



2 Efficient power consumption

3 Appropriate aerodynamic shape

1 Optimised structural design



PROJECT-BASED EDUCATION ON DIGITAL DESIGN. TBW DESIGN

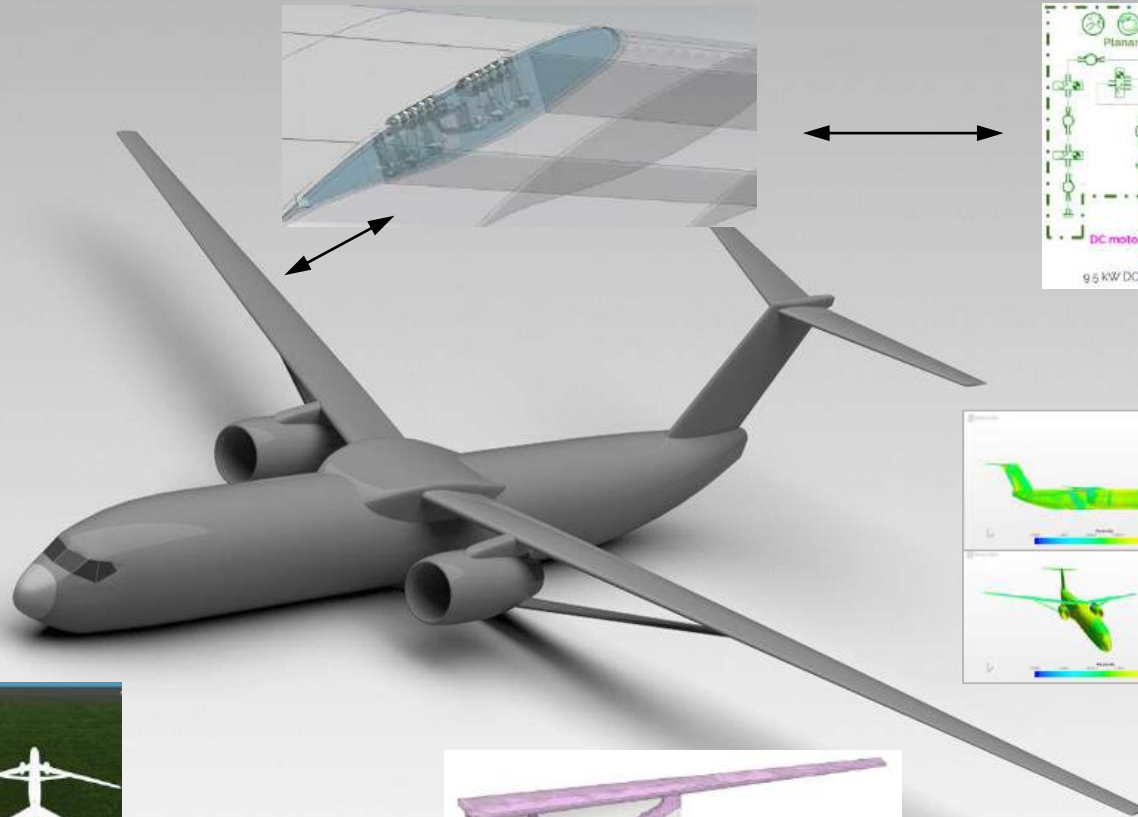
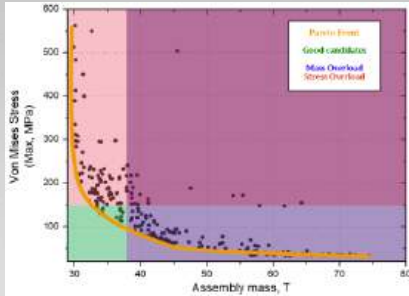
Flight distance: 5700 km

Wing span: 45 m

Hybrid turbofan

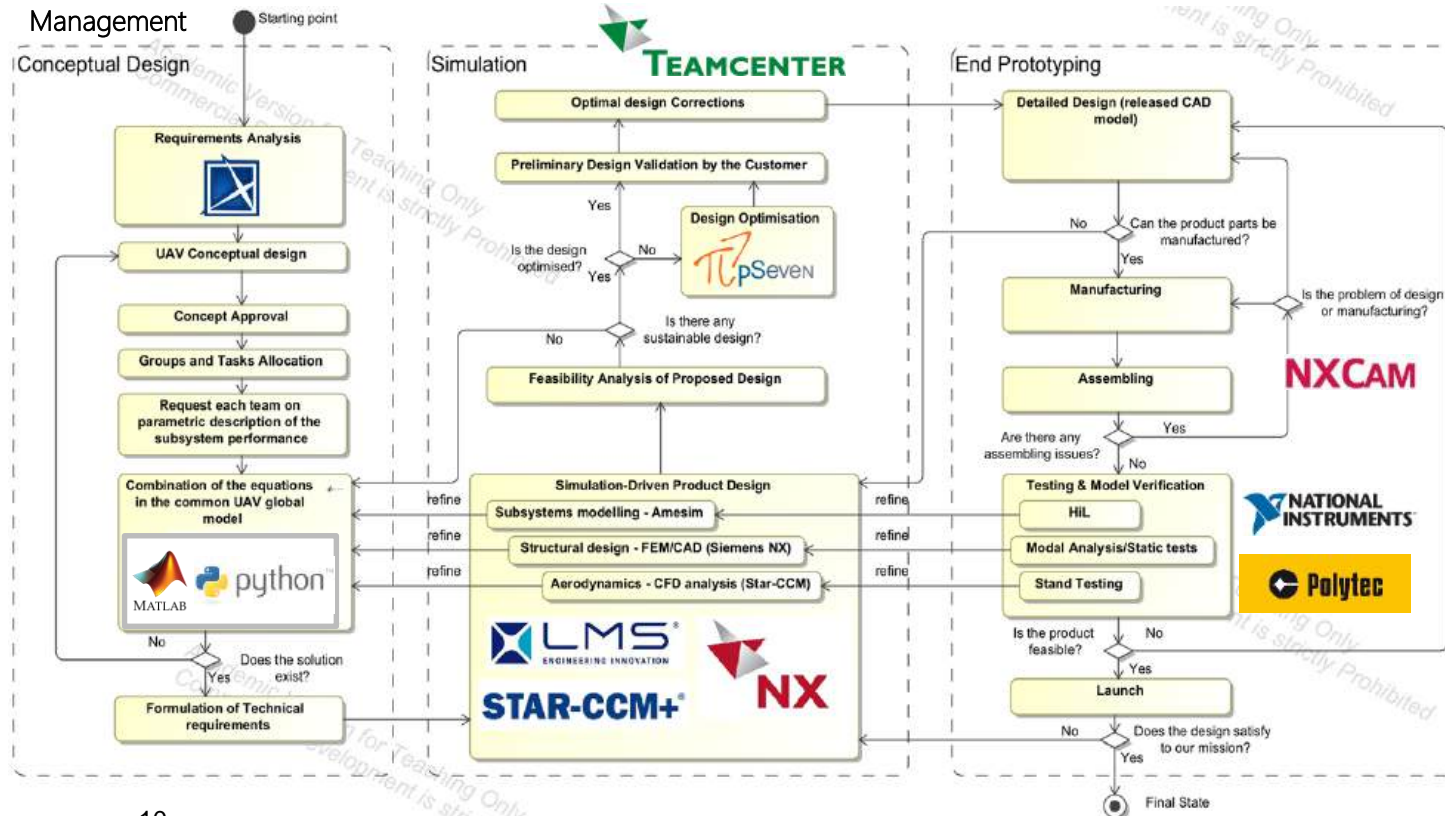
Thrust: 190 kN

Fuel consumption: 3400 kg/hour



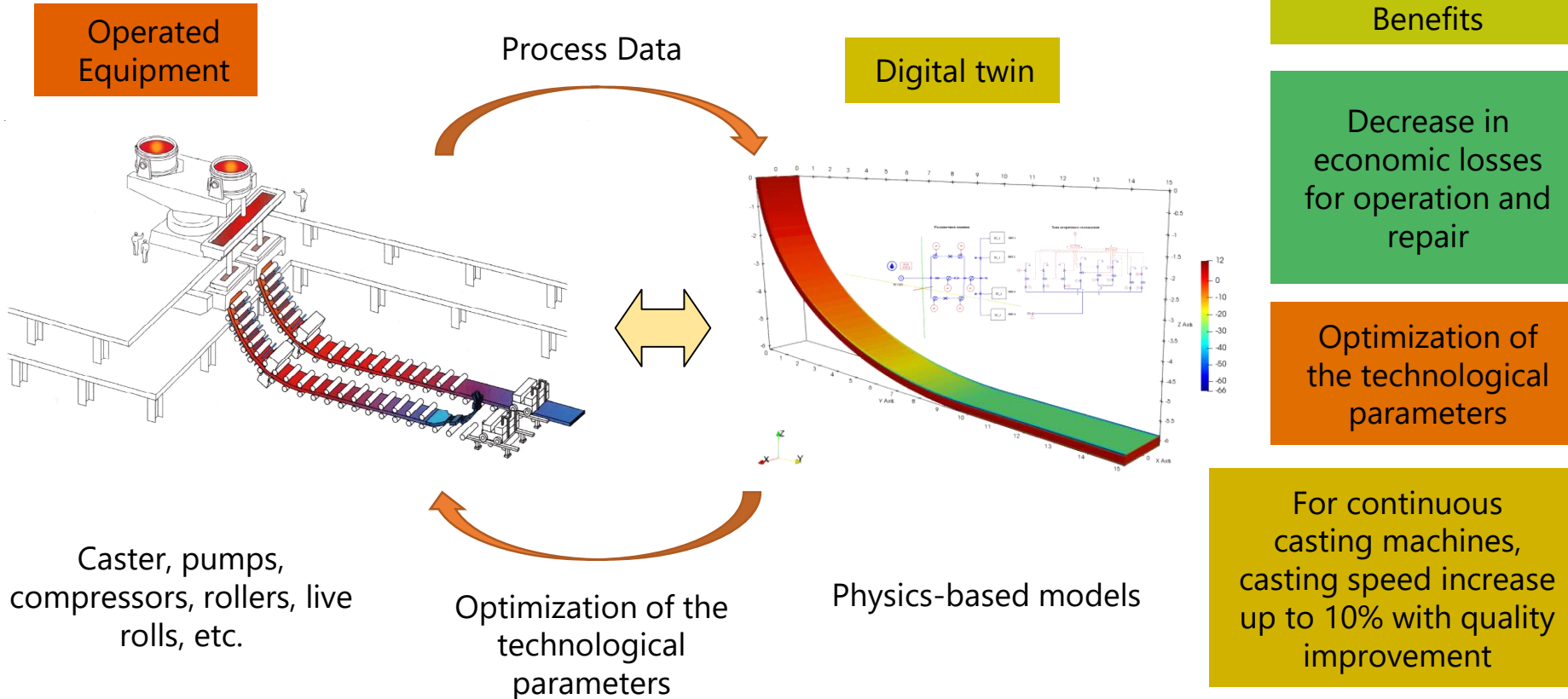
DIGITAL DESIGN WORKFLOW

Data & Processes Management

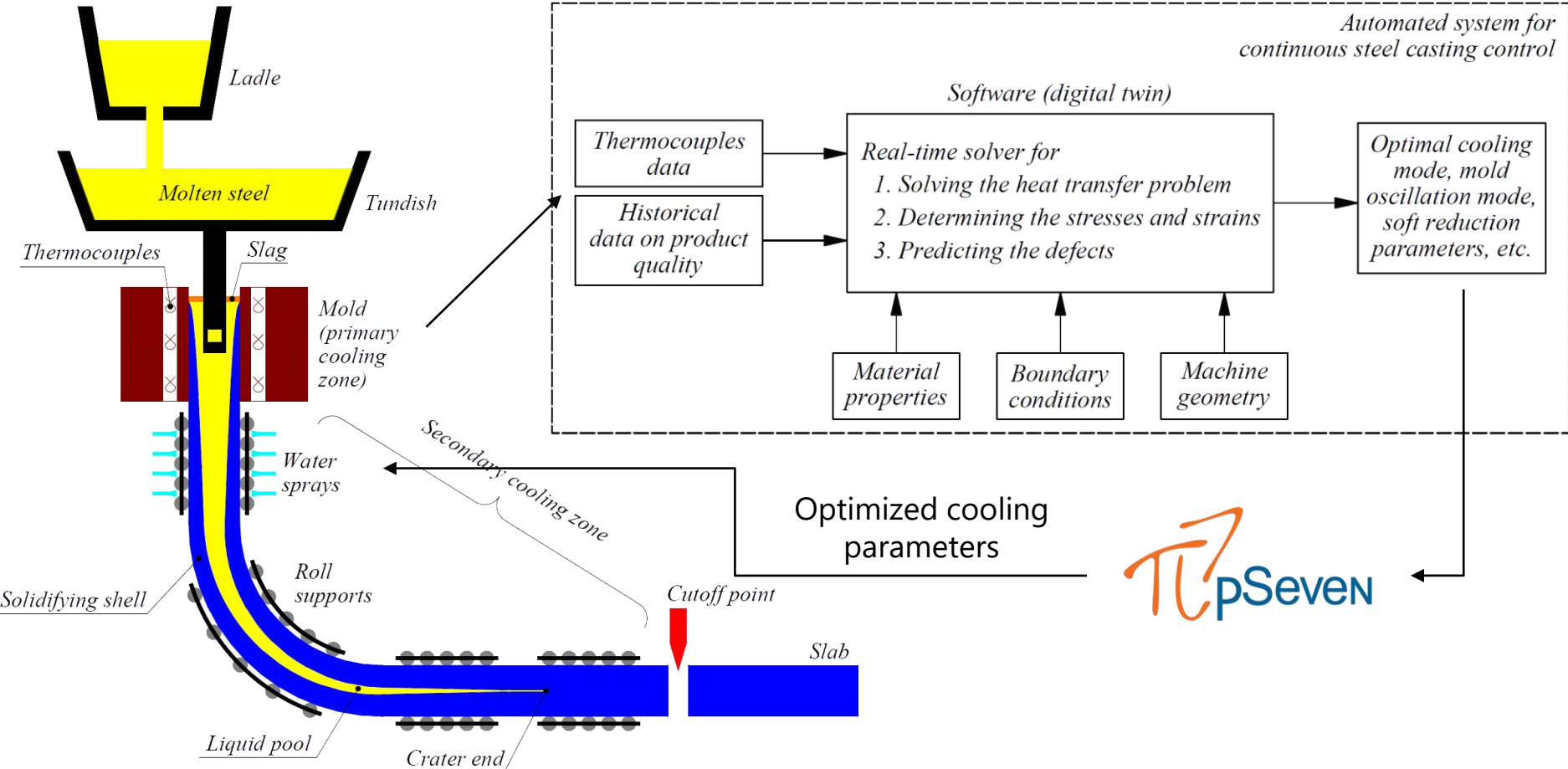


CONTINUOUS CASTING OF A STEEL. SECONDARY COLING ZONE OPTIMIZATION

DIGITAL TWIN IN METALLURGY INDUSTRY



APPLICATION OF DIGITAL TWINS IN MODERN STEELMAKING



MODELS AND ALGORITHMS: HEAT TRANSFER PROBLEM

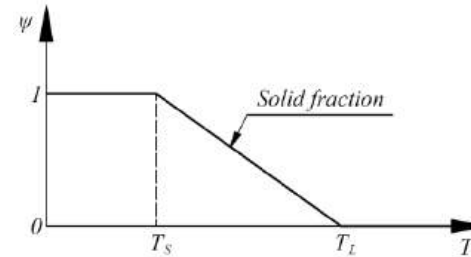
I. Fourier-Kirchhoff equation

$$\rho c \left(\frac{\partial T}{\partial t} + (\vec{v} \cdot \vec{\nabla}) T \right) = \vec{\nabla} \cdot (k \vec{\nabla} T) + q_v$$

$$\chi(T) \triangleq \frac{\rho}{k} v \left(c + \frac{\lambda'}{T_L - T_S} \right)$$

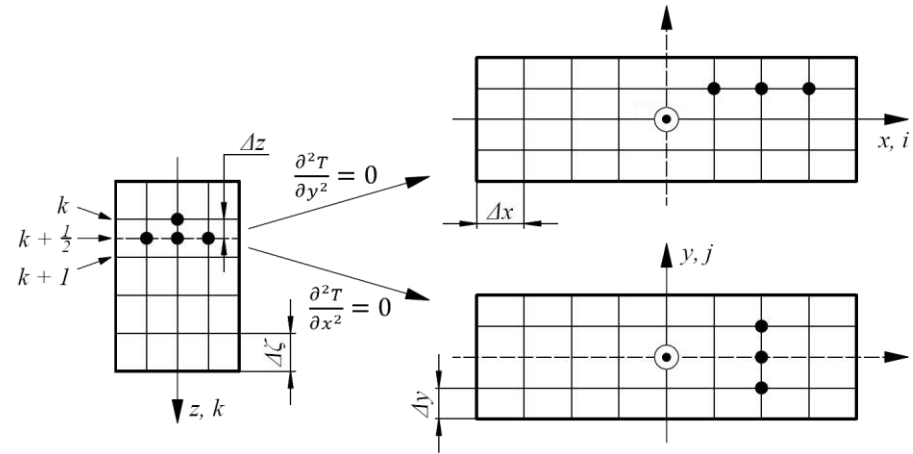
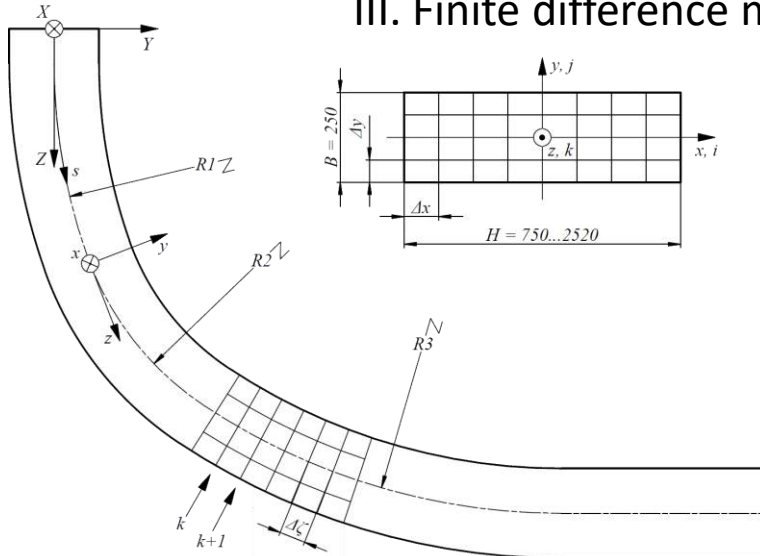
$$\chi \frac{\partial T}{\partial z} = \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2}$$

II. Considering the phase change



$$\rho = \psi \rho_S + (1 - \psi) \rho_L$$

III. Finite difference method (FDM) scheme and stencils



MODELS AND ALGORITHMS: PREDICTION OF CRACKS

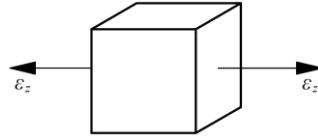
I. Considered components of strain

$$\varepsilon = \varepsilon_z = \varepsilon_0 - \alpha y = \varepsilon^e + \varepsilon^t + \varepsilon^c$$

Elastic strain $\rightarrow \varepsilon^e = \frac{\sigma}{E}$

Thermal strain $\rightarrow \varepsilon^t = \alpha \Delta T$

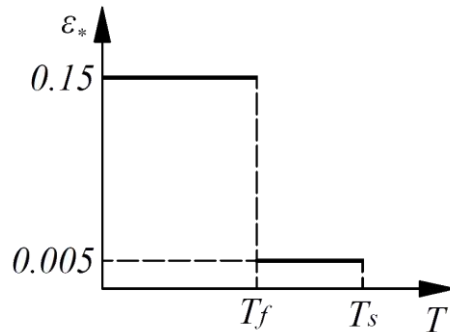
Creep strain $\rightarrow \varepsilon^c = \int \xi^c dt$



III. Damage accumulation

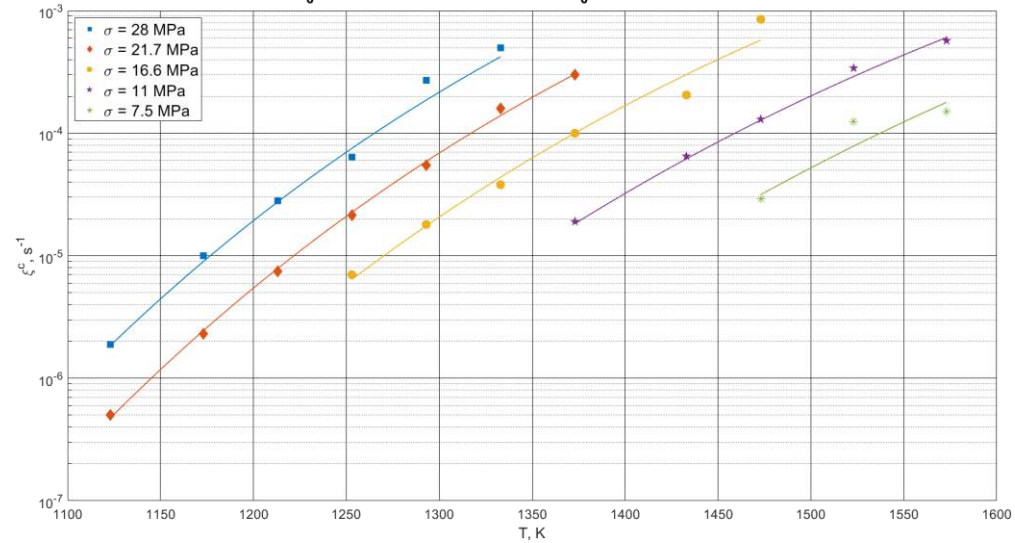
$$\Delta \omega = \frac{\Delta t}{t_f}$$

$$t_f = \frac{\varepsilon_*(T)}{\xi^c}$$



II. Creep strain rate formula

$$\xi^c = A * \exp(-T_0/T) * \sigma^{n+kT}; A = 58769999322, T_0 = 62648, n = 10.731, k = -0.004802$$



PRELIMINARY RESULTS: SOFTWARE

```

INPUT file
1 MP, TEMP, L, 1536
2 MP, TEMP, S, 1496
3 MP, LAMBDA, 84000
4 MP, DENS, L, 6500
5 MP, DENS, S, 7000
6 MP, KX, L, 34.5
7 MP, KX, S, 35
8 MP, CX, L, 720
9 MP, CX, S, 700
10 MP, EMIS, 0.7
11 MP, EX, 50000000000
12 MP, ALP, 0.00002
13
14 TB, FRAG, 100
15 TB, EPS, MAX, 0.15
16 TB, EPS, MIN, 0.005
17
18 BC, ALPHA, AIR, 20
19 BC, ALPHA, WATER, 1000
20 BC, ALPHA, STEAM, 500
21 BC, ALPHA, ROLLS, 1800
22
23 BC, TEMP, AIR, 30
24 BC, TEMP, WATER, 40
25 BC, TEMP, STEAM, 200
26 BC, TEMP, ROLLS, 450
27
28 BC, MOLD, FLUX, 1500000
29 BC, MOLD, FALL, 0.5
30 BC, MOLD, CORNER, 0.05
31
32 INIT, TEMP, 1540
33
34 GEOM, INGOT, LEN, 1.54
35 GEOM, INGOT, WID, 0.25
36
37 GEOM, MACH, STR, 1
38 GEOM, MACH, FURN, 4
39 GEOM, MACH, RS, 10
40 GEOM, MACH, RE, 6
41
42 GEOM, MOLD, LEN, 1.1
43
44 GEOM, ROLL, DIAM, 0.3
45 GEOM, ROLL, DIST, 0.37
46 GEOM, ROLL, CONT, 0.005
47
48 GEOM, COOL, LEN, 12
49 GEOM, COOL, SPR, 0.12
50
    
```

Digital Twin

Program

CSC Preprocessor

Use default input data

Read input data from file

Heat transfer solver type Implicit Explicit

DX step (mm)

DY step (mm)

DZ step (mm)

DZ substep (mm)

Section part Full Half Quarter

Validate mesh

Generate input data file

CSC Mesh



Step (mm) Nodes Elems

X

Y

Z

Time substep (s)

Max timestep (s)

Req RAM (GB)

Export machine contour

CSC Solver

Calculate strain rate/stress

Calculate strain

Calculate damage accum

If dam acc reaches 1 Destroy elem Continue

Number of threads

Solve

CSC Postprocessor

Layers Elements

Temperature
Solid fraction
Strain rate
Stress
Damage acc

Total strain
Elastic strain
Thermal strain
Creep strain

Export 3D results

Export 2D results

Export data for furnace

Furnace

Use CSC data and results

Read input data from file

Read init temps from file

Heat transfer solver type Implicit Explicit

Range (s) Steps SSteps

Air

Furn

SX (mm) SY (mm) SZ (mm)

Time substep (s)

Max timestep (s)

Req RAM (GB)

Solve

Export results

Log

```

16:36:57 | Program has started
CSC 'Input', 'Options' and 'Output'
clusters created
Available RAM: 128 GB

16:37:03 | CSC | PREP | Validating mesh
Solver disabled
'Input' cluster renewed
'Mesh' cluster created
Done. Solver enabled

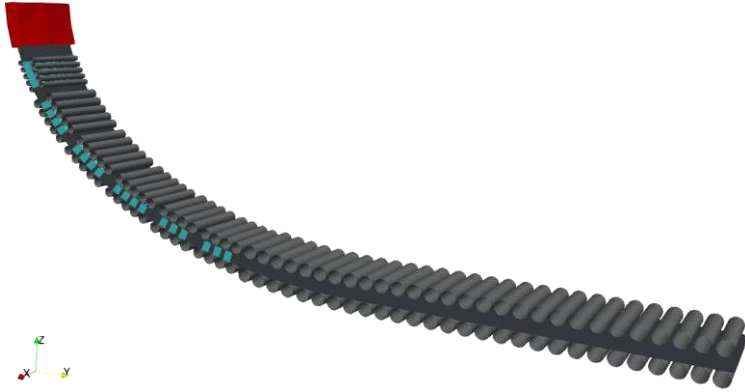
16:37:10 | CSC | SOL | Solution has started
Output disabled
'Results' cluster created
Elapsed time: 0:07:22
Done. Output enabled

16:44:59 | CSC | POST | Exporting 2D data
(2XT) Done

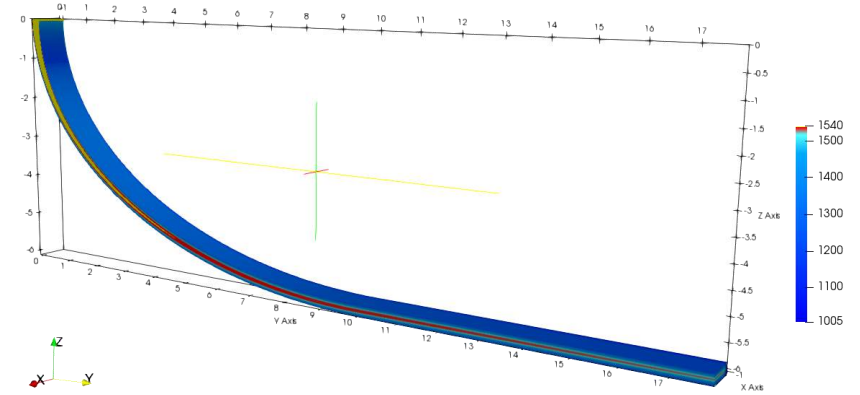
16:45:17 | CSC | POST | Exporting 3D data
(VTR) Done
    
```

CALCULATION RESULTS

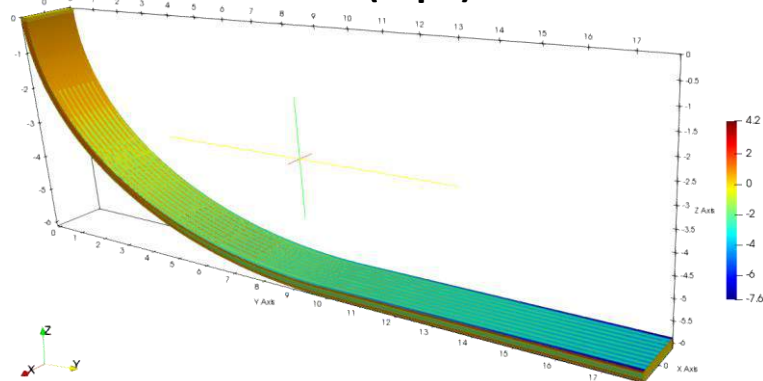
Continuous casting machine with rollers



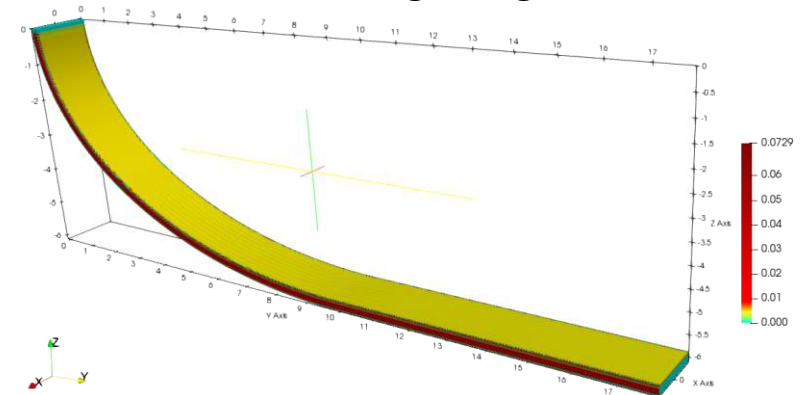
Temperature distribution (C)



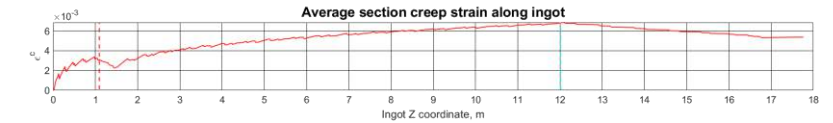
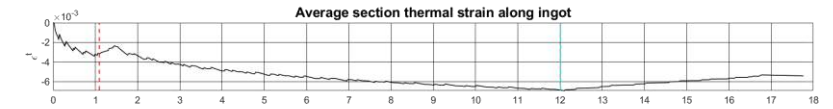
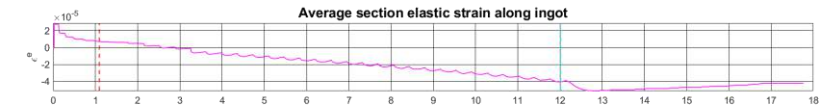
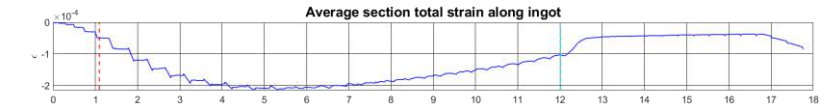
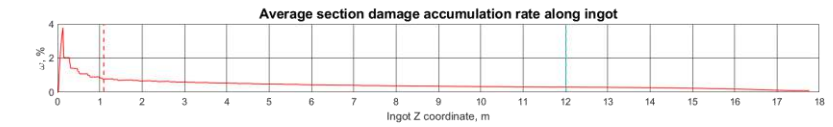
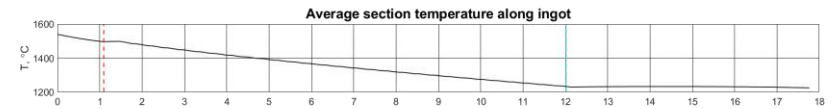
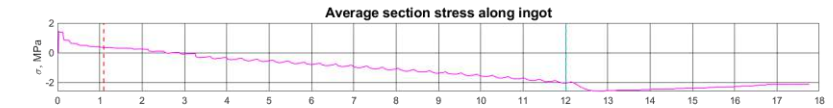
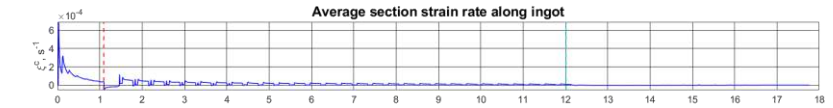
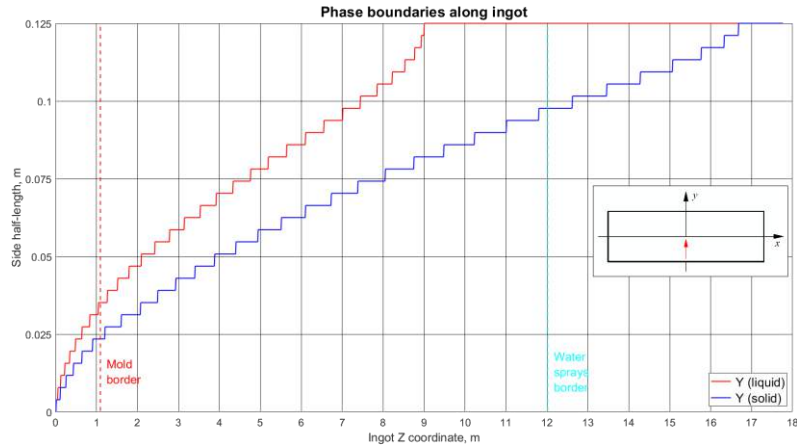
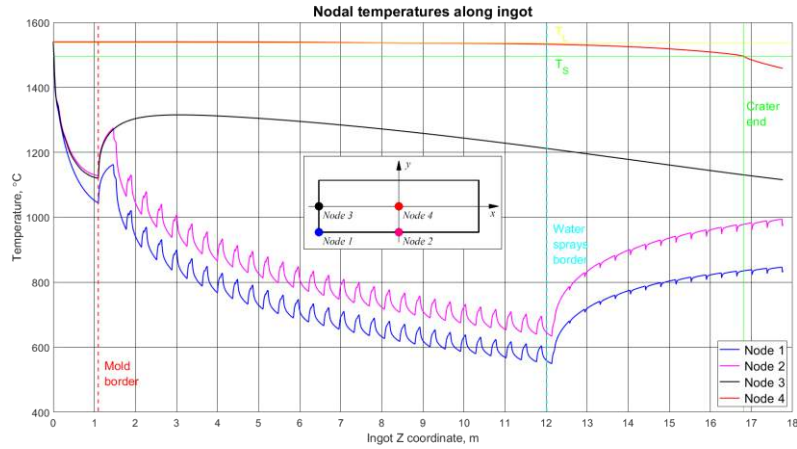
Stress (Mpa)



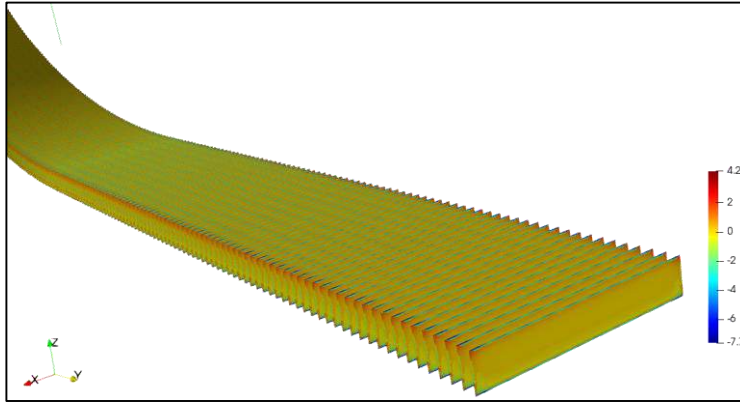
Damage range



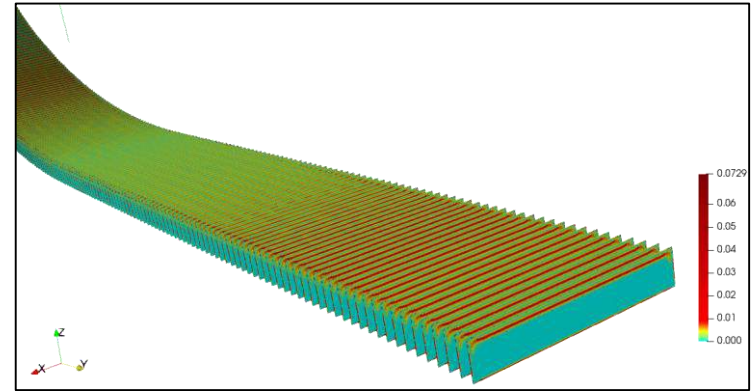
PRELIMINARY RESULTS: 2D PLOTS



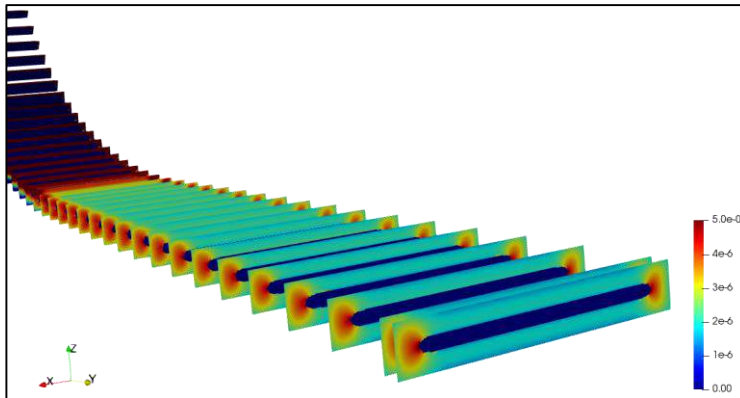
Stress in section (MPa)



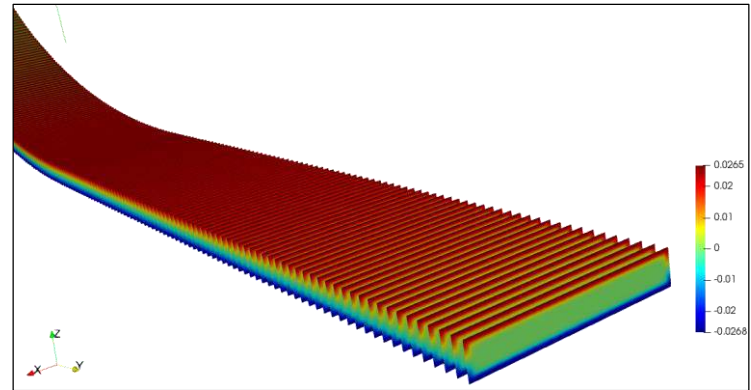
Damage



Strain rate (sec⁻¹)



Full strain



OPTIMIZATION RESULTS

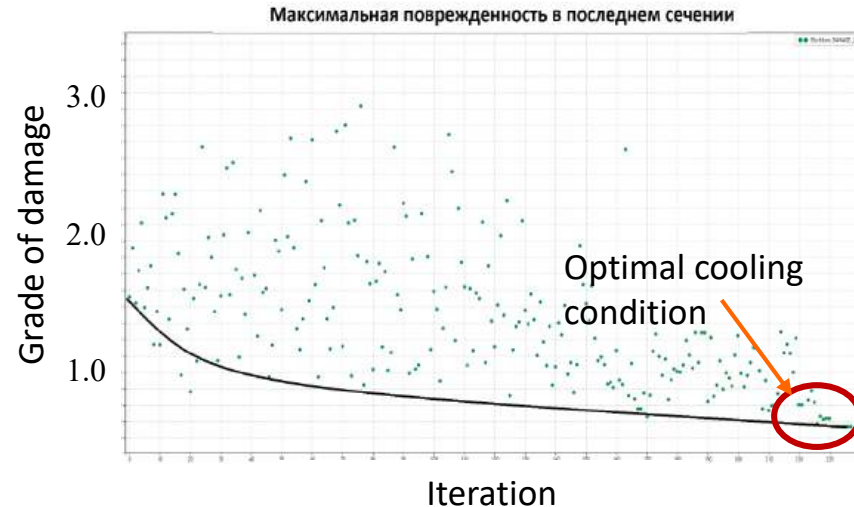
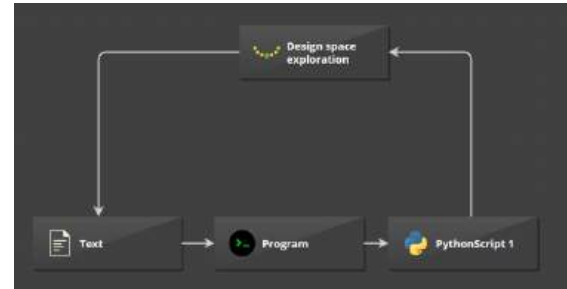
Calculation of the optimal heat removal mode in the SCZ for a casting speed of 1 m / min:

- The starting point is the data of water consumption in the SCZ for casting speeds of 0.6 - 1.0 m / min;
- Specific steel.

Results:

- Potential of optimization.
- Improving quality from **1.5 to 1** grade of damage

Simple Workflow



Maximum damage in the last section

TRUSS BRACED WING AIRCRAFT STUDENT PROJECT

Team of Introduction to PLM 2019

MBSE team

Hekmat Taheri Nejad



Yana Brovar



Hamed Jafarzadeh



Fahimeh Shiravani



Wing structure team

Ishwarchandra Gulgule



Kirill Minchenkov



Eugene Statnik



Bogdan Tonanaiskii



SDPM team

Guillaume Debaille



Karolina Latserus



Alexander Matkov



Vitaly Petrov



Production system team

Arzu Kurgan



Artur Kolesnikov



Svetlana Okoyomova



Mikhail Pustovgarov



Aerodynamics team

Ekaterina Isachenko



Yaroslav Nasonov



Flight Dynamics team

Aleksandr Filimonov



Vadim Leshchev



Artem Yakimchuk



Folding team

Denis Galagan



Vladislav Solovyev



Denis Sopichev



Propulsion team

Igor Usachev



Igor Yatsenko



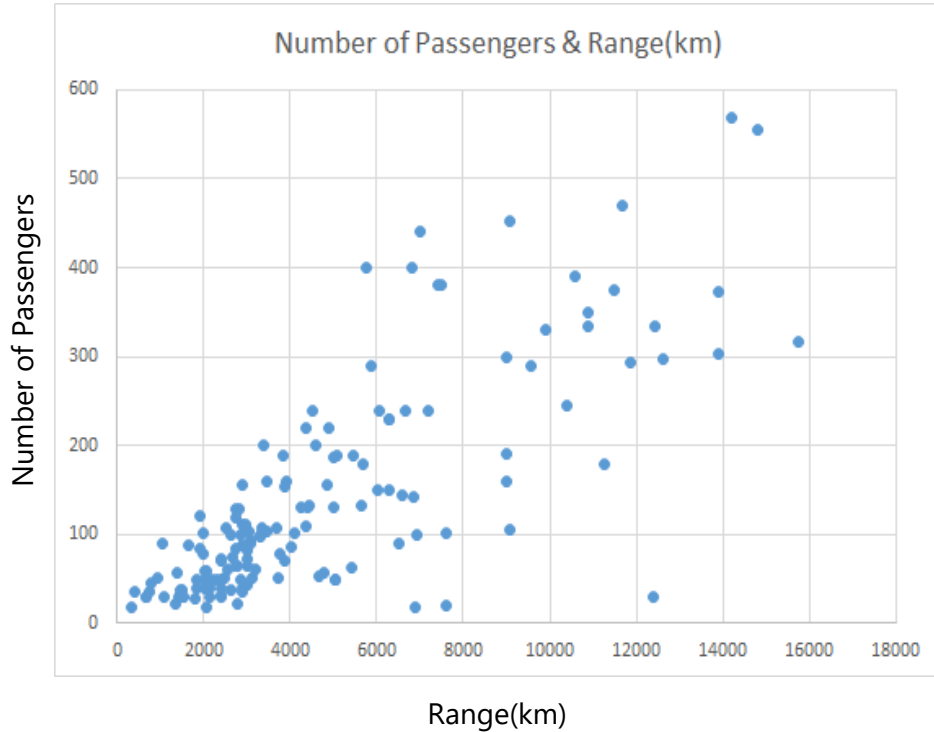
Andrey Zogov



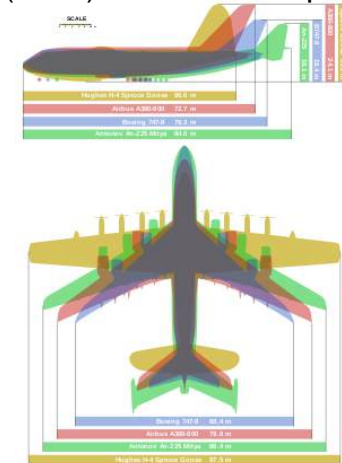
Mikhail Raevskiy



MBSE(Comparative study)

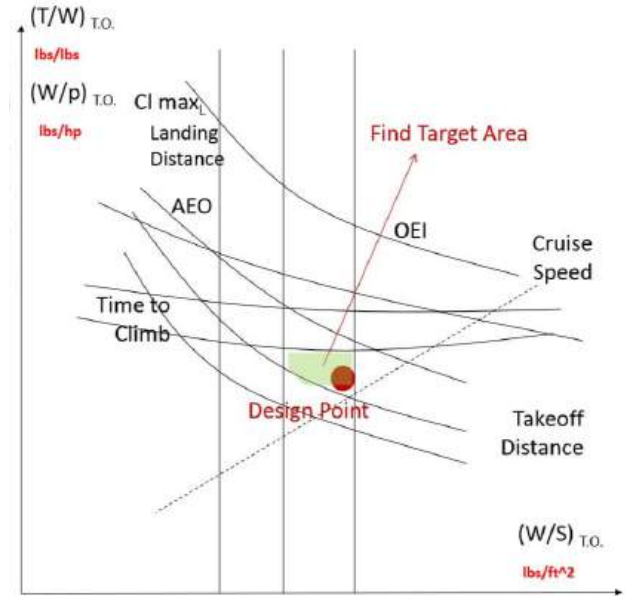


Boeing SUGAR Truss-Braced Wing (TBW) Aircraft Concept *



MBSE (Preliminary sizing)

| | |
|-----------|--|
| W_TO | 77110 kg |
| Range | 5700 km |
| W/S | 456 kg/m ² ~ 94 lb/m ² |
| T/W | 0.4 |
| CD0 | 0.0132 |
| Wing Span | 51.8 m |
| Wing area | 111.5 m ² |



Thrust over weight ratio vs. Wing loading

SPDM - Simulation and optimization framework

1st level

High-level wing structure & aerodynamics

MBSE

Boeing 737 geometry

Folding

Mass of mechanism

Aerodynamics

Wing and truss geometry variables

MATLAB
Aerodynamics model

 piSeven

Design of Experiment

2nd level

Wing structure & stress analysis

Manufacturing

Materials

PLM Software
SIEMENS NX

Wing structure & stress 3D model

 piSeven

Design of Experiment

3rd level

Flight dynamics

LMS Amesim

Flight dynamics model

 piSeven

Design of Experiment

Flight distance

Wing and truss geometry estimation
Airplane mass estimation

Lift coefficients

Precised geometry of wing and truss

Engine weight estimation
Fuel consumption

 piSeven
Optimization

Surrogate model

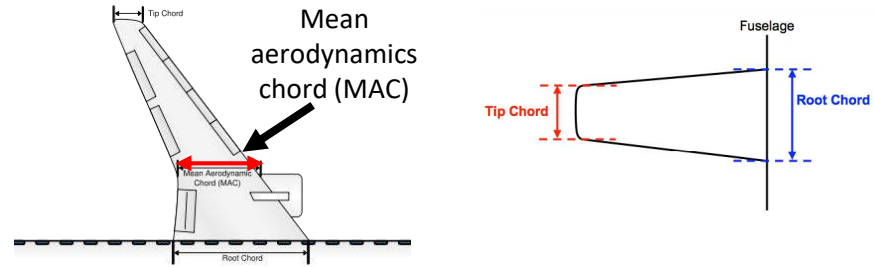
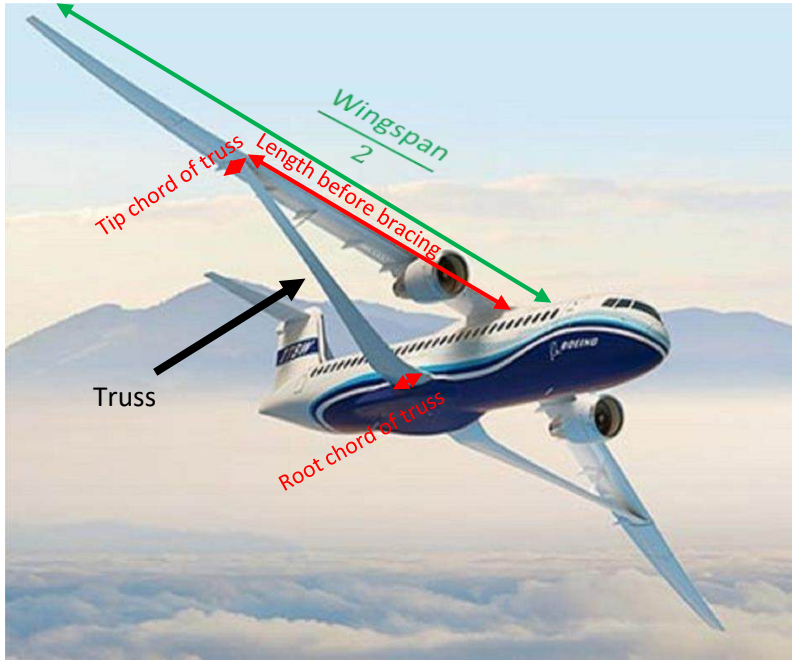
Maximize flight distance (>5700 km)

Minimize stresses in wing and truss

Minimize fuel consumption

Optimized design space

SPDM - 1st level optimization: general idea



$$\text{Truss taper ratio} = \frac{\text{Root chord of truss}}{\text{Tip chord of truss}}$$

Our goal is **to maximize the flight distance** (to fit the requirement of flight distance ≥ 5700 km) and to **minimize the total mass of aircraft**

| Parameter | Interval of variation |
|--------------------------|-----------------------|
| Truss taper ratio | [1; 5] |
| Length before bracing, m | [9; 14] |
| Wing span, m | [35; 60] |
| Truss root chord, m | [1; 5] |

SPDM - 1st level optimization: results

Parallel plots on optimized parameters

Flight distance, km

TakeOff mass, kg

Length before bracing, m

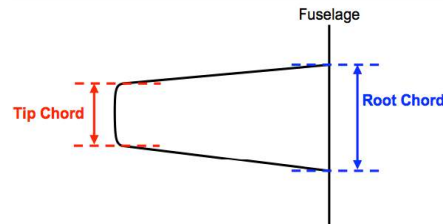
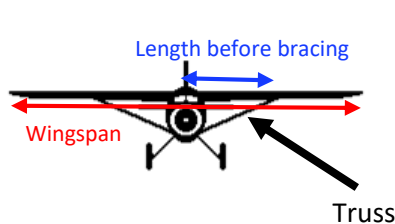
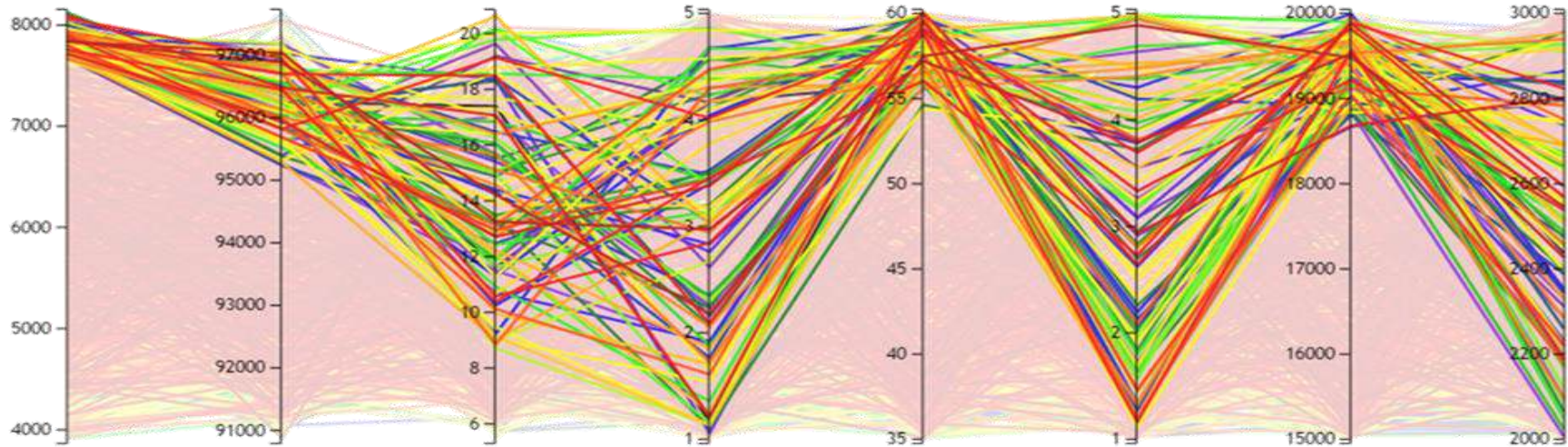
Truss root chord, m

Wingspan, m

Truss taper ratio

Mass of fuel, kg

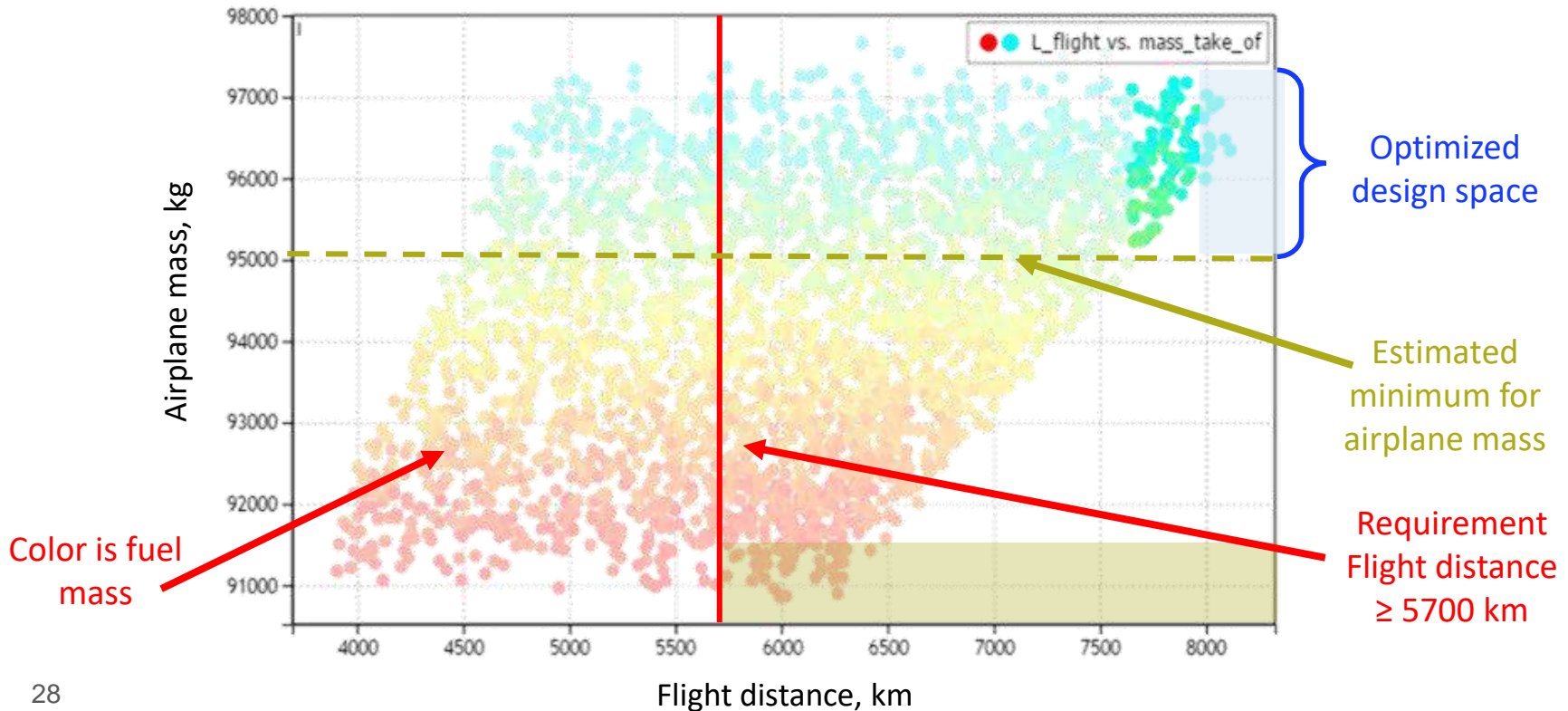
Mass of engine, kg



$$\text{Truss taper ratio} = \frac{\text{Root chord of truss}}{\text{Tip chord of truss}}$$

SPDM - 1st level optimization: results

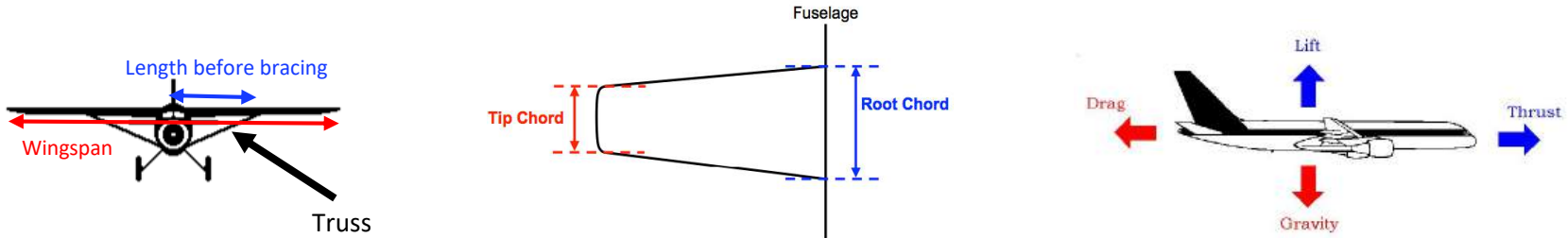
Dependency of airplane mass on flight distance



SPDM - 1st level optimization: results

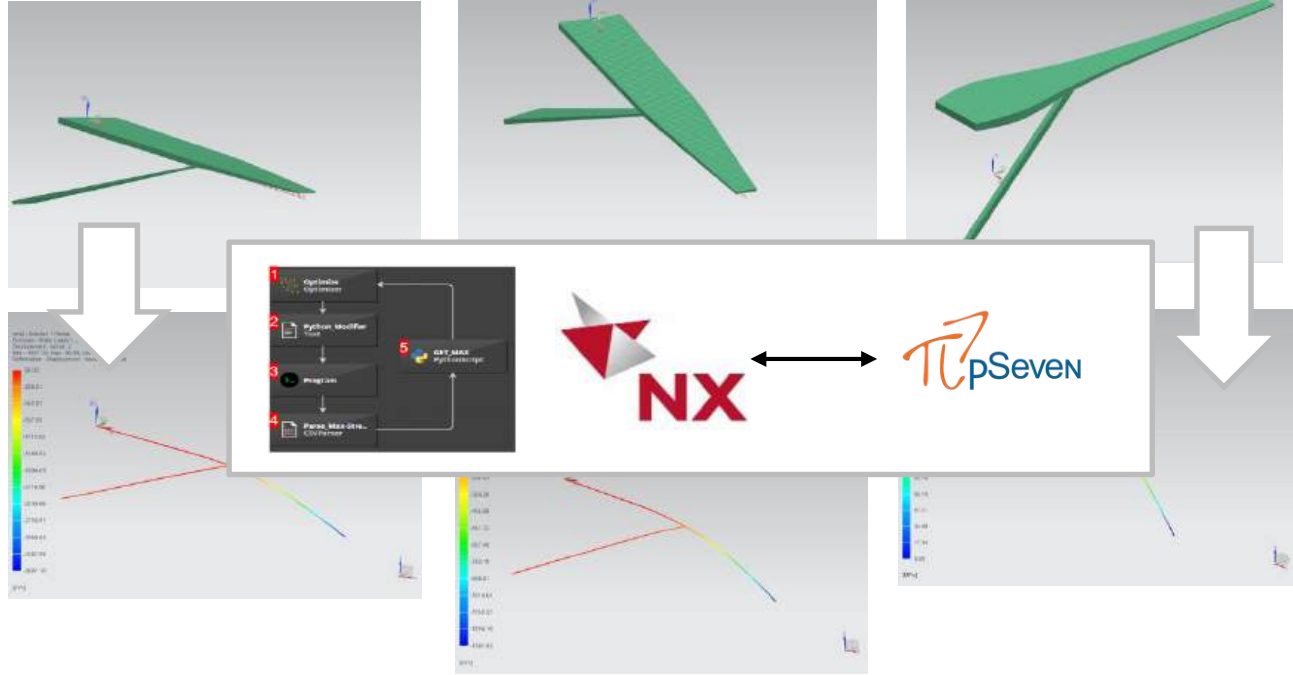
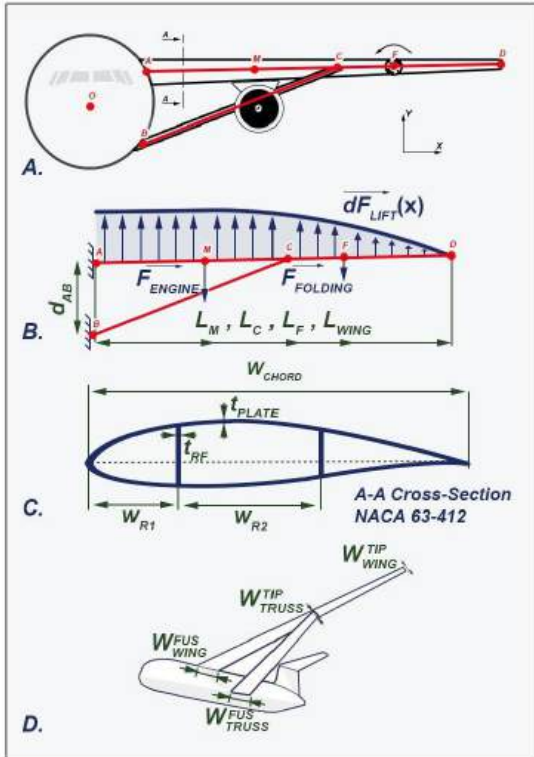
Optimized parameter from the high level model

| Length of flight, km | Take-Off Mass, kg | Length before bracing, m | Truss root chord, m | Truss taper ratio | Wingspan, m | Mass of fuel, kg | Mass of engine, kg |
|----------------------|-------------------|--------------------------|---------------------|-------------------|-------------|------------------|--------------------|
| 8114 | 96343 | 15.0 | 4.10 | 1.83 | 59.9 | 19905 | 2391 |
| 8057 | 96934 | 10.6 | 2.84 | 3.69 | 59.0 | 19813 | 2568 |
| 8088 | 96469 | 17.0 | 1.21 | 2.62 | 59.5 | 19871 | 2593 |



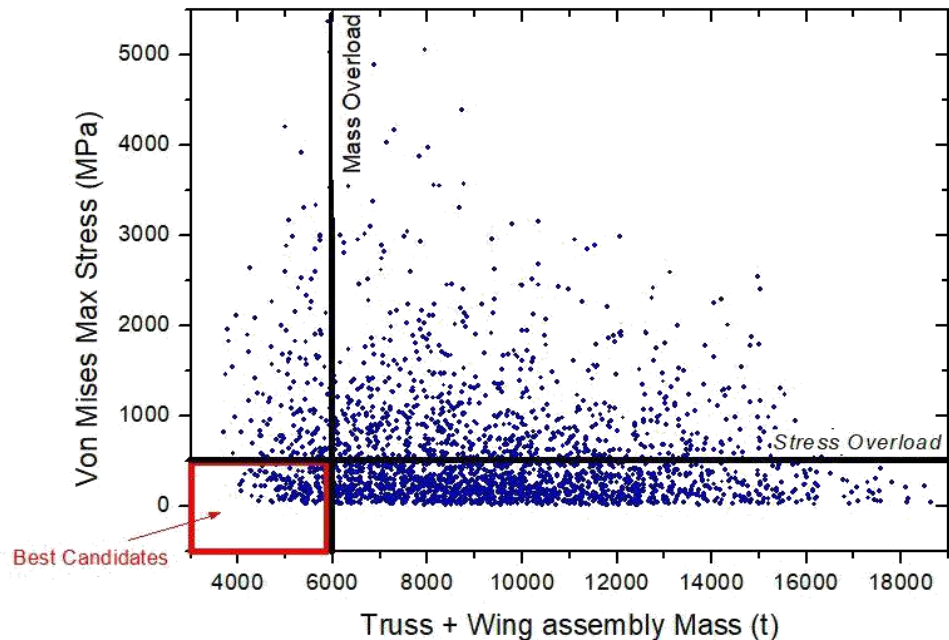
$$\text{Truss taper ratio} = \frac{\text{Root chord of truss}}{\text{Tip chord of truss}}$$

SPDM - 2nd level optimization: generative algorithm for structure



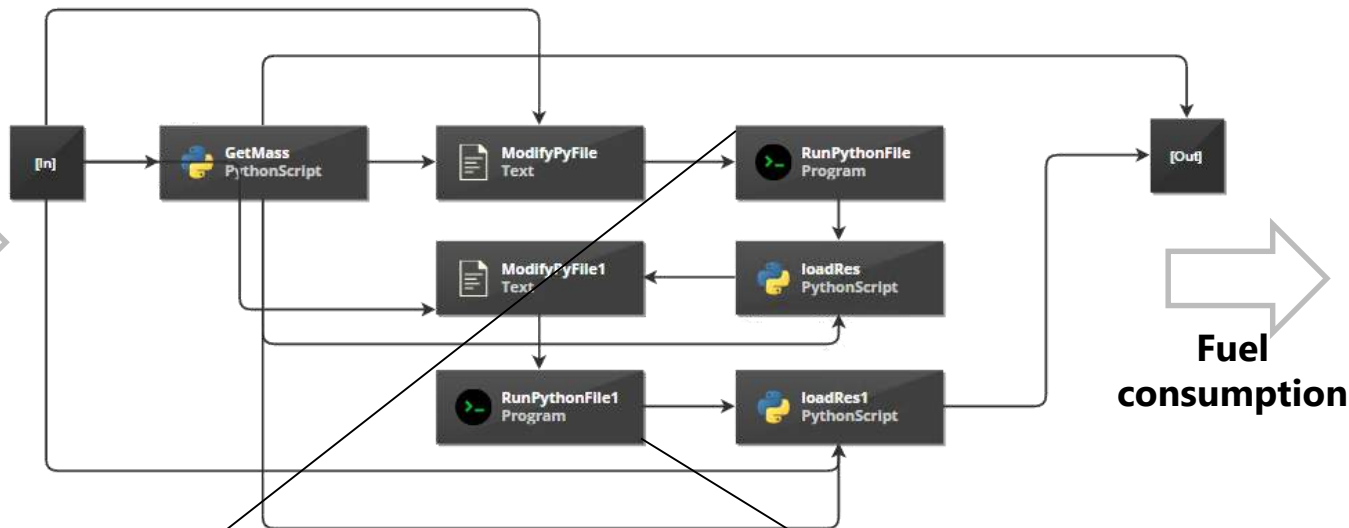
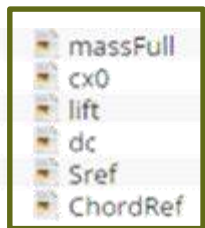
SPDM - 2nd level optimization: generative algorithm for structure

| Data Exchange Parameters | Structural Inputs for each pre-filtered candidate | | | |
|----------------------------|---|----------------------|---|-----------------------|
| | Unit | Symbol | Description | Exchange |
| Engine Weight | N | \vec{F}_{ENGINE} | Weight of the Engine | Exchanged Scalar |
| Folding Weight | N | $\vec{F}_{FOLDING}$ | Weight of the folding mechanism | Fixed scalar (4500 N) |
| Folding Mechanism Position | m | L_f | Position of the folding mechanism | Exchanged Scalar |
| Truss Fixation position | m | L_c | Position of the truss fixation on main wing | Exchanged Scalar |
| Truss Taper Ratio | N/A | TR_{TRUSS} | $= \frac{W_{TRUSS}^{FUS}}{W_{TRUSS}^{TIP}}$ | Exchanged Scalar |
| Wing Taper Ratio | N/A | TR_{WING} | $= \frac{W_{WING}^{FUS}}{W_{WING}^{TIP}}$ | Exchanged Scalar |
| Truss root chord | m | W_{TRUSS}^{FUS} | Width of truss at fuselage position | Exchanged Scalar |
| Wing root chord | m | W_{WING}^{FUS} | Width of wing at fuselage position | Fixed Scalar (6 m) |
| Truss wing distance | m | d_{AB} | Distance between wing and truss in the fuselage cross-section plane | Fixed Scalar (4 m) |
| Wingspan | m | L_{WING} | Wingspan of the plane ($2 \cdot L_{WING} + D_{Fuselage}$) | Exchanged Scalar |
| Lift | N/m | $d\vec{F}_{LIFT}(x)$ | Distributed load of the lift forces in horizontal flight multiplied by a Safety factor of 3 | Exchanged Vector |
| Fuselage Radius | m | $D_{Fuselage}$ | Radius of the fuselage | Fixed (6m) |



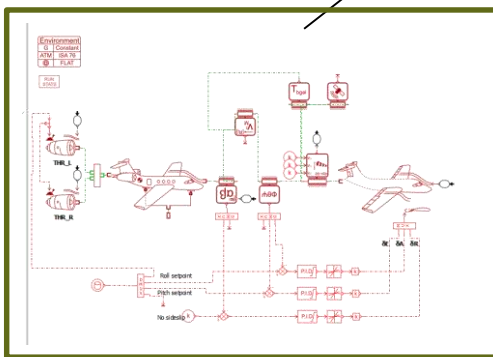
SPDM - 3rd level optimization: workflow

Initial parameters from high level model

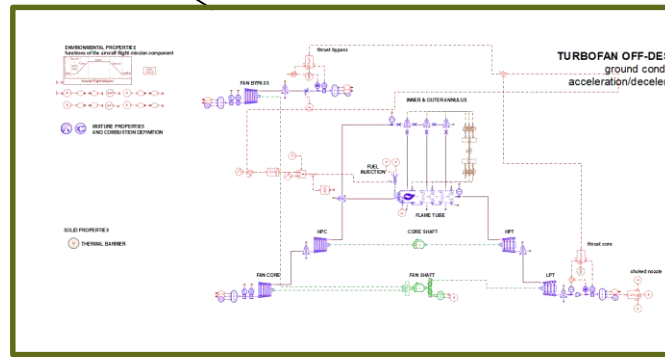
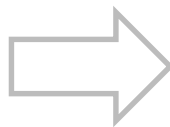


Fuel consumption

Amesim Model of Flight Dynamics



Required thrust force

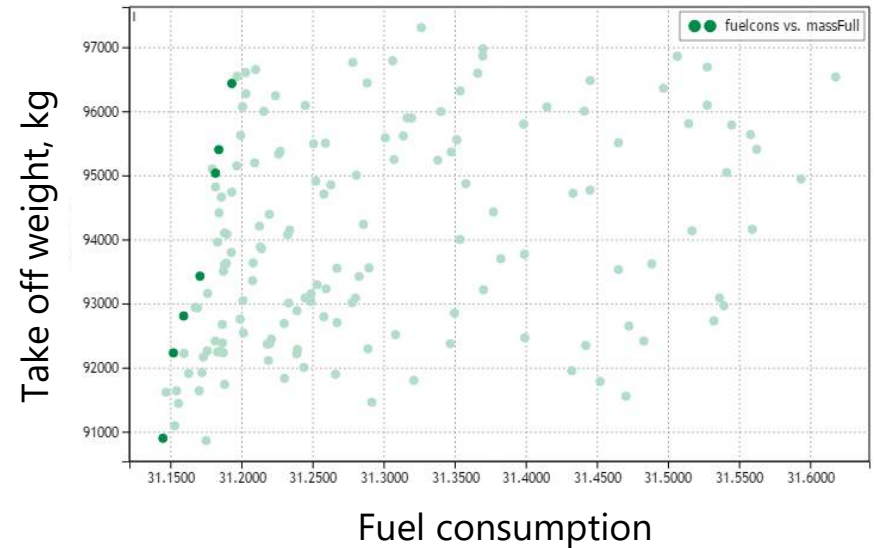
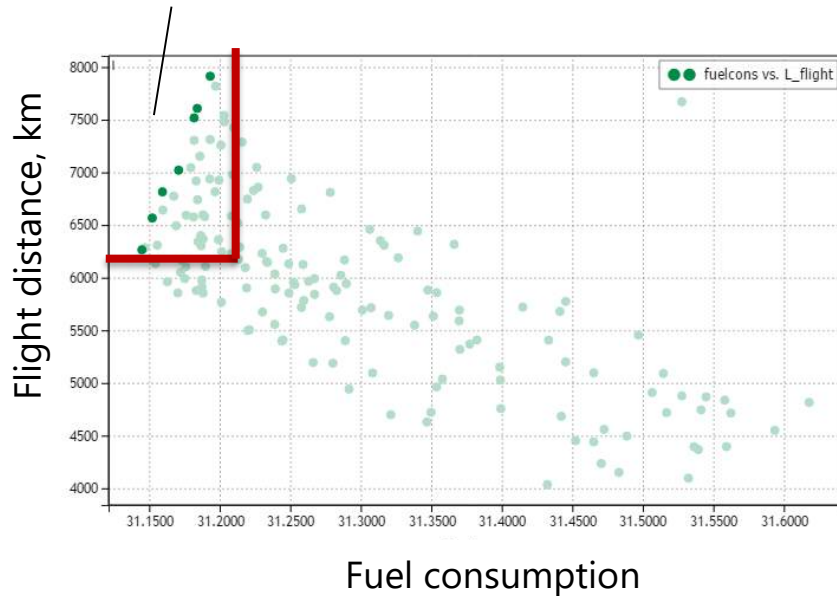


Amesim Model of Engine

Results of optimization

- Results are based on the DOE with initial sample evaluation

Optimal zone



Best design: flight distance = **7912** km ToM = **96433** kg

Optimized on **38 %**

NUMERICAL SIMULATION OF CRACKING DURING PULTRUSION OF LARGESIZE PROFILES

Numerical simulation of cracking during pultrusion of largesize profiles

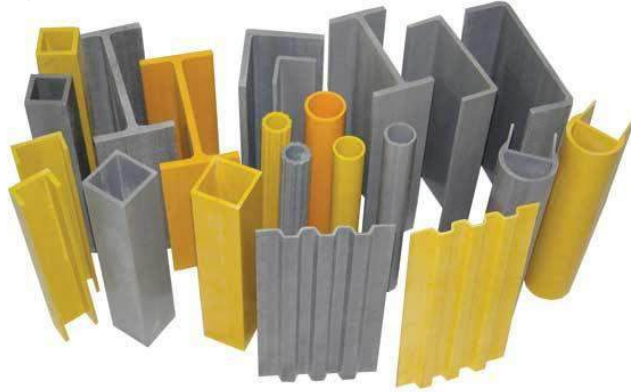
Alexander Safonov, Mikhail Gusev, Anton Saratov, Iskander Akhatov

Center for Design, Manufacturing and Materials,
Skolkovo Institute of Science and Technology, Moscow, Russia

22nd International Conference on Composite Structures and
1st Chinese Conference on Composite Structures
Wuhan, China
02 Nov 2019



Applications & Main challenges



Industry

- *Construction*
- *Corrosion resistance*
- *Electrical applications*
- *Marine*
- *Transportation*
- *Sport and Leisure*

Advantages

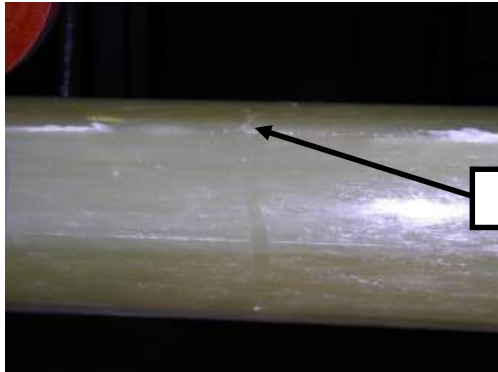
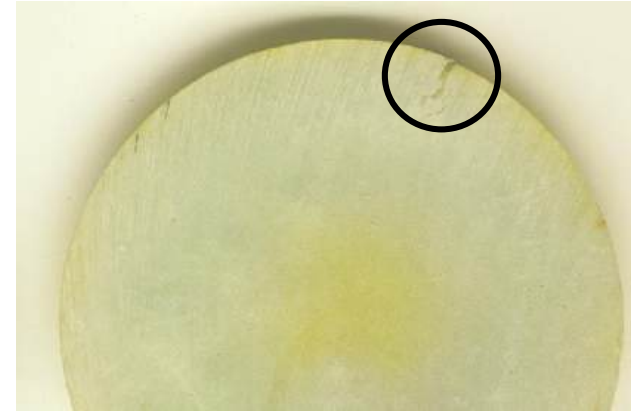
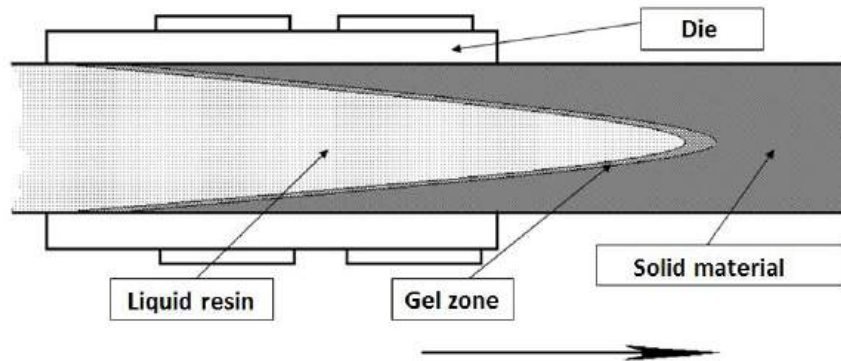
- Light weight
- High strength
- Fatigue resistance
- Ease of installation
- Corrosion resistance
- Fire performance
- Easy maintenance
- Insulating properties

Challenges, Main reasons, Physics involved

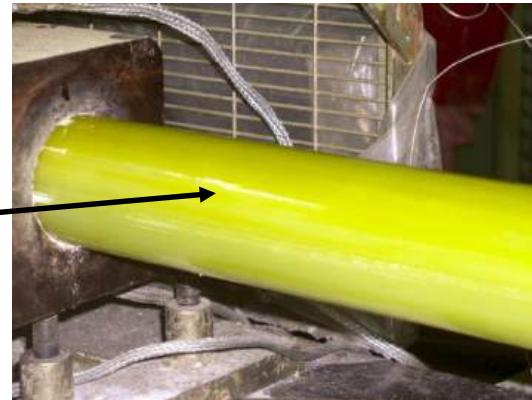
- Peak temperature and degree of cure evolution
- Exothermic chemical reaction during curing
- Heater configurations
- Type of resin matrix system
- Geometry of the die
- Geometry of the resin injection chamber
- Phase transformations
- Anisotropic permeability of the fibre reinforcement
- Residual stresses and shape distortions
- Crack & void formations
- Pulling force
- Fibre misalignment

Safonov AA, Carlone P, Akhatov I. Mathematical simulation of pultrusion processes: A review. Composite Structures 2018;184. doi:10.1016/j.compstruct.2017.09.093

Pultrusion of large diameter rods (80 mm)



Crack



Pulling speed – 5 cm/min

Process simulation

- Heat transfer $\rho_c C_{pc}(T, \alpha) \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial x^2} + k \frac{\partial^2 T}{\partial y^2} + q,$
- Curing of resin $\frac{d\alpha}{dt} = A_0 \exp\left(-\frac{E_a}{RT}\right) (1 - \alpha)^n$
- Stress-strain distribution

Cure-hardening/instantaneously linear elastic (CHILE) approach

$$E_m(T^*) = \begin{cases} E_m^0, & T^* < T_{C1} \\ E_m^0 + \frac{T^* - T_{C1}}{T_{C2} - T_{C1}} (E_m^\infty - E_m^0), & T_{C1} \leq T^* \leq T_{C2}, \\ E_m^\infty, & T^* > T_{C2} \end{cases}$$

$T^* = T_g - T$, T_g – glass transition temperature depending on degree of cure

$$T_g(\alpha) = T_{g0} + (T_{g\infty} - T_{g0}) \frac{\lambda \alpha}{1 - (1 - \lambda) \alpha}$$

The model is implemented in ABAQUS using the user-subroutines: HETVAL, UEXPAN, UMAT, FILM, URDFIL, UFIELD, UEXTERNALDB

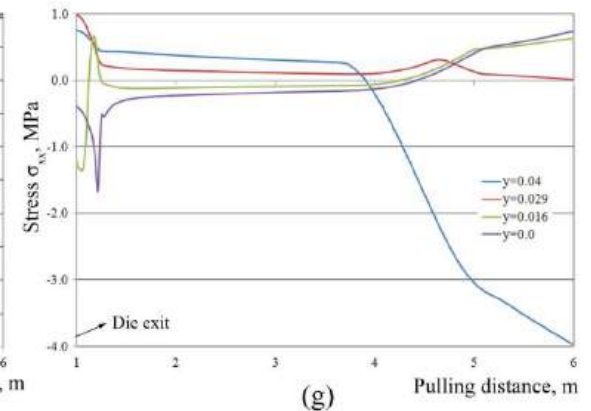
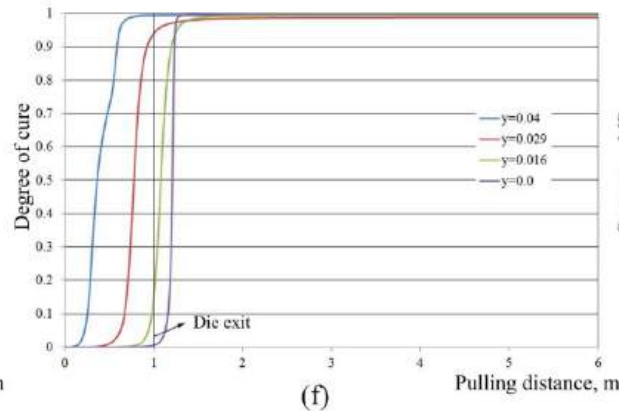
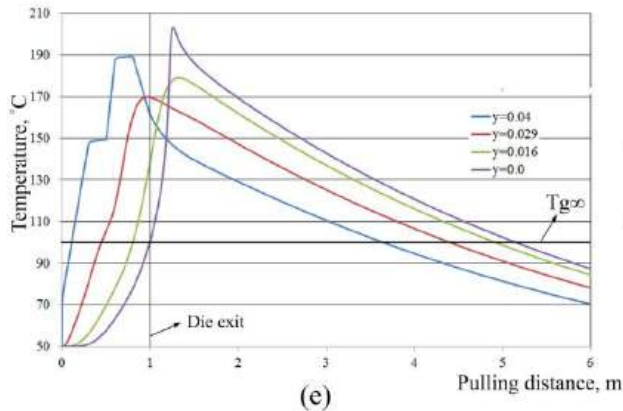
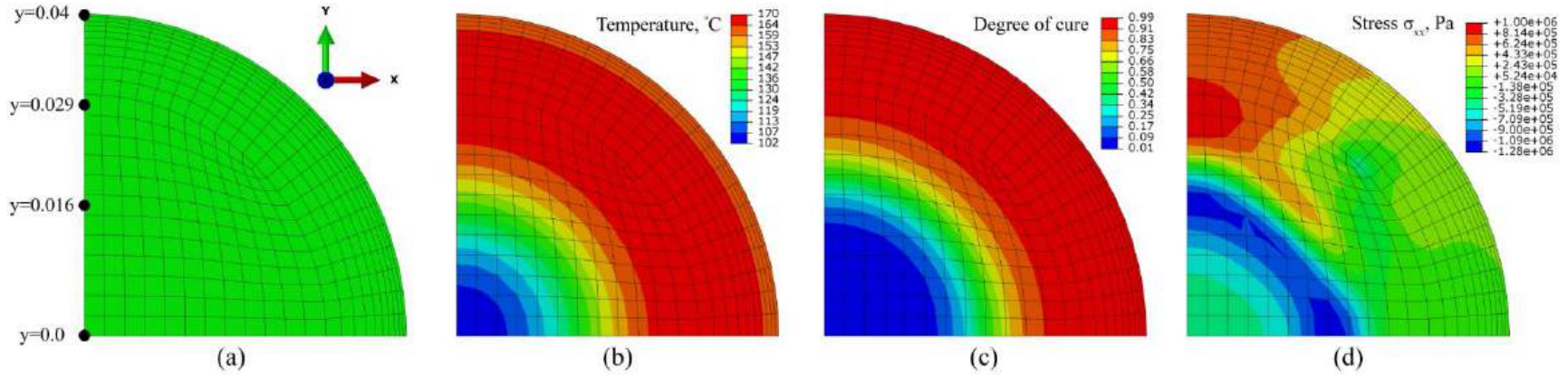
2D transient heat equation in the Lagrangian frame

G.L. Batch, C.W. Mocosko. Heat transfer and cure in pultrusion: model and experimental verification, *AIChE Journal*, 39, 7, 1993, pp. 1228-1241

2D plane strain model

I. Baran, C.C. Tutum, M.W. Nielsen, J.H. Hattel, Process induced residual stresses and distortions in pultrusion, *Composites Part B: Engineering*, 51, 2013, pp. 148-161

Simulation results in section after die exit



Optimization. Problem statement

Optimization parameters:

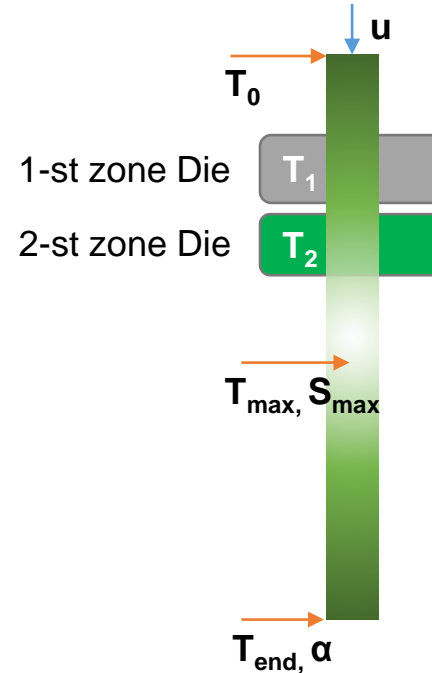
- Initial temperature of mixture, T_0
- Die 1-st zone temperature, T_1
- Die 2-nd zone temperature, T_2
- Pulling speed, u

Objective function of one criterion optimization:

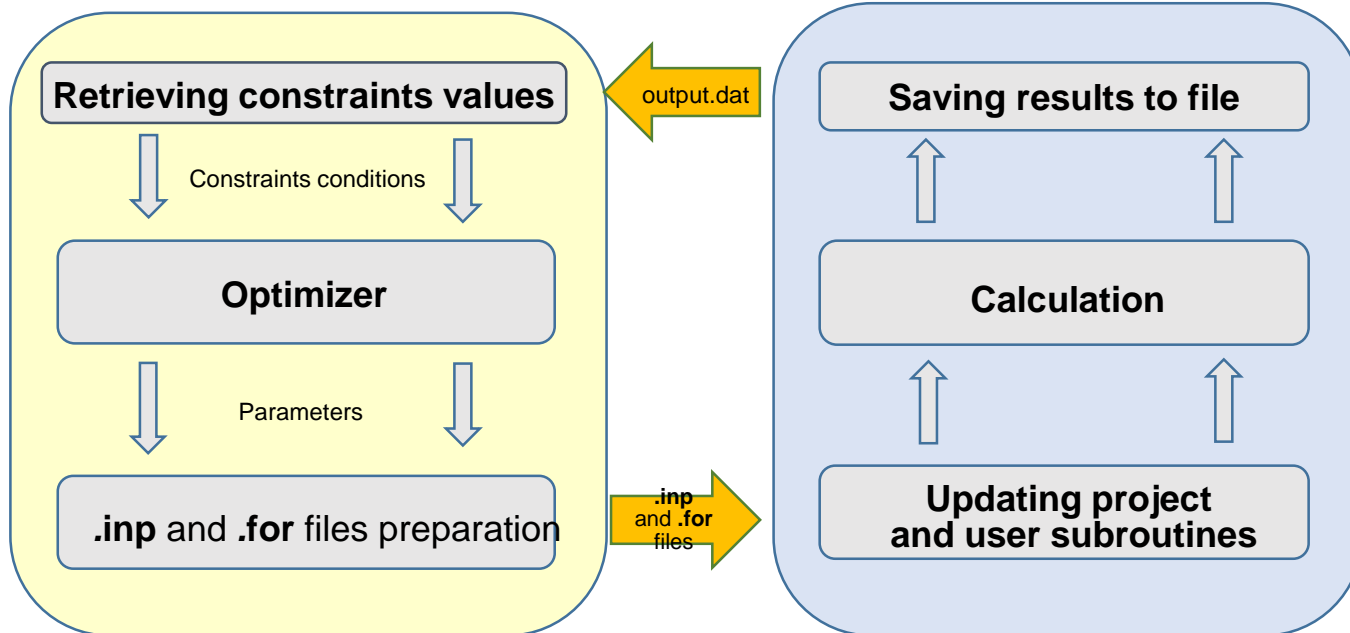
- Pulling speed $u \rightarrow \max$

Constraints:

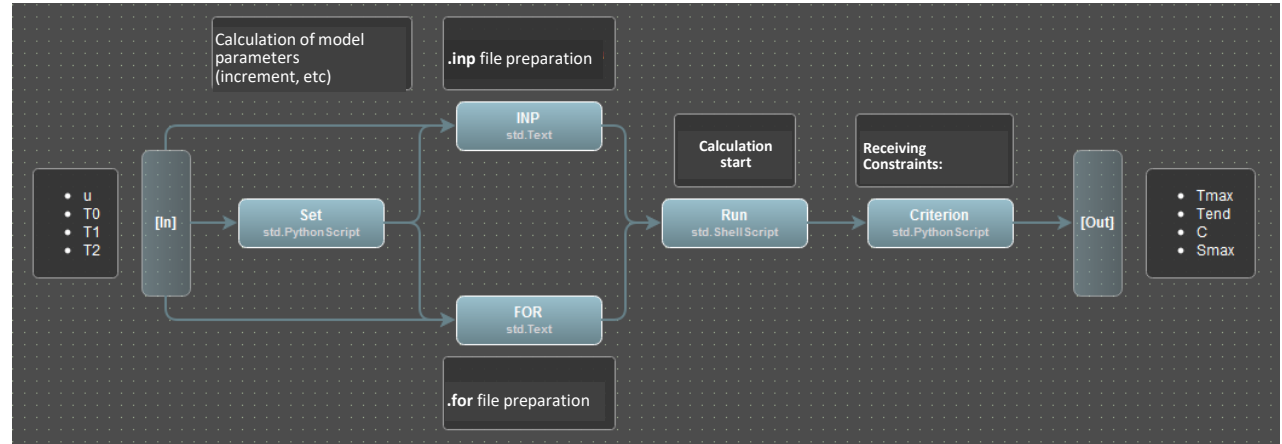
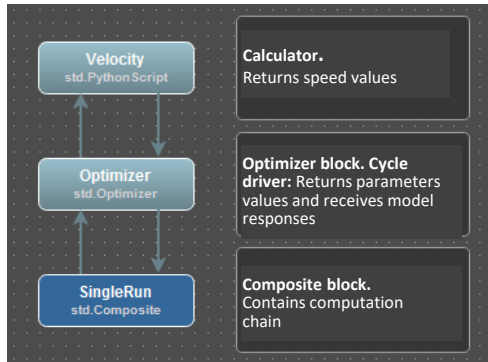
- Transverse stress in pultruded rod, S_{\max}
- Maximum temperature of material, T_{\max}
- Maximum temperature at the end section, T_{end}
- Degree of polymerization at the end section, α



General Workflow



pSeven. Workflow



- Single-criterion optimization problem: **SBO** (surrogate-based optimization) method
- Four constraints

Best point

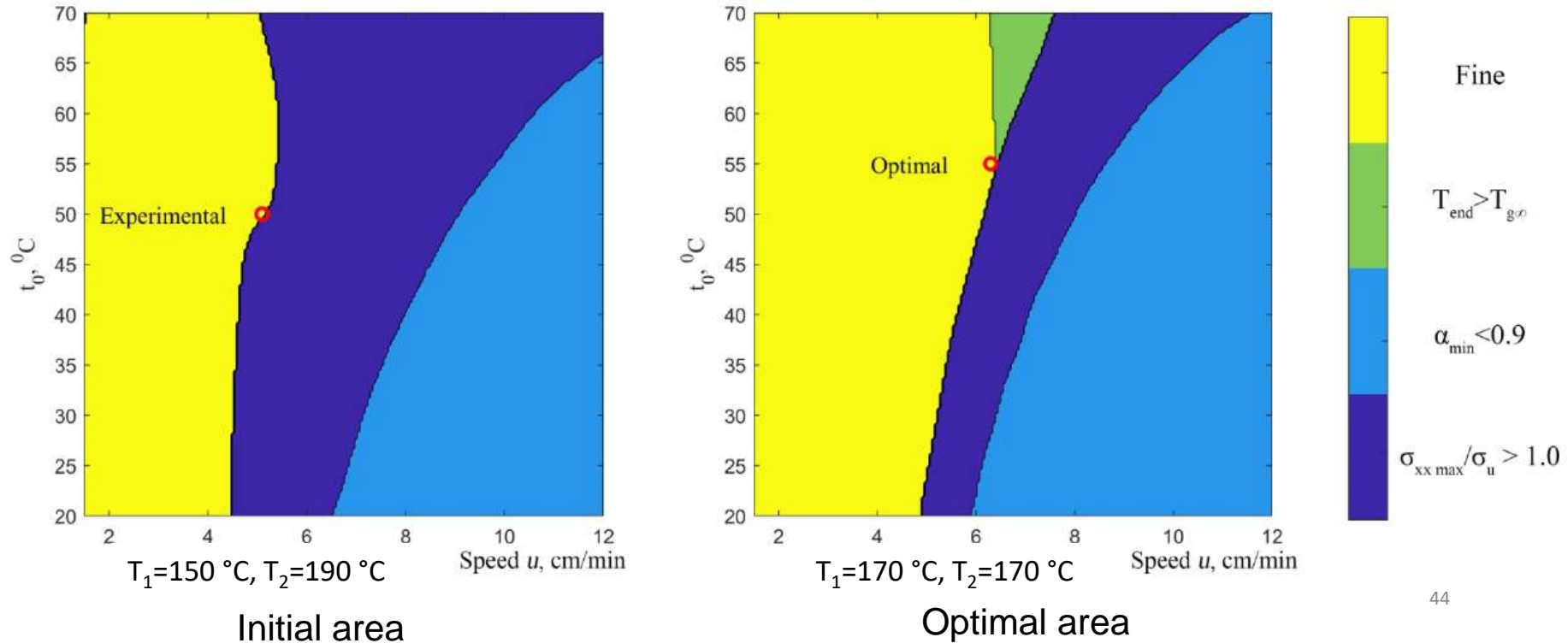
Initial vs Optimum configuration comparison

| | Parameters | | | | Constraints | | | |
|------------|--------------|------------|------------|------------|----------------|----------------|----------------|------------------------------|
| | u , cm/min | T_0 , °C | T_1 , °C | T_2 , °C | T_{end} , °C | T_{max} , °C | α_{min} | $\sigma_{xx_{max}}/\sigma_u$ |
| Boundaries | - | 20-70 | 120-170 | 150-200 | <101.5 | <210.0 | >0.90 | <1.0 |
| Initial | 5.0 | 50 | 150 | 190 | 87.6 | 202.9 | 0.99 | 0.99 |
| Optimum | 6.0 | 55 | 170 | 170 | 101.4 | 203.0 | 0.97 | 0.95 |

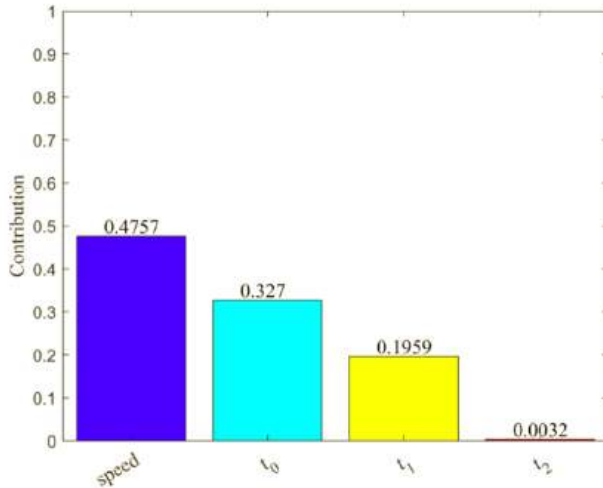
Achieved **20%** of increasing the pulling speed

Computation results. Approximation model

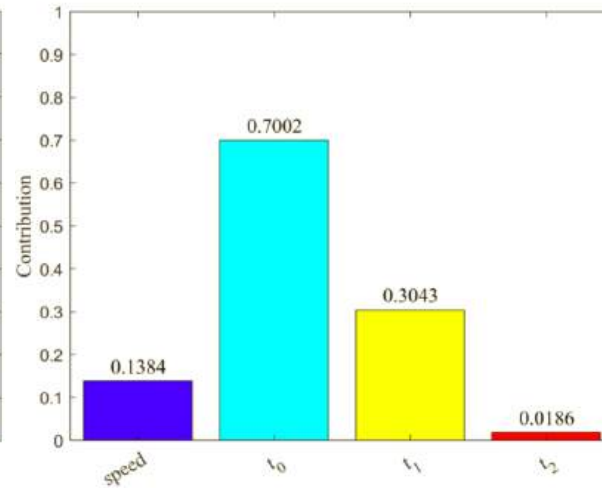
Contour plot with boundary restrictions for Initial and Optimal area based on Surrogate Model



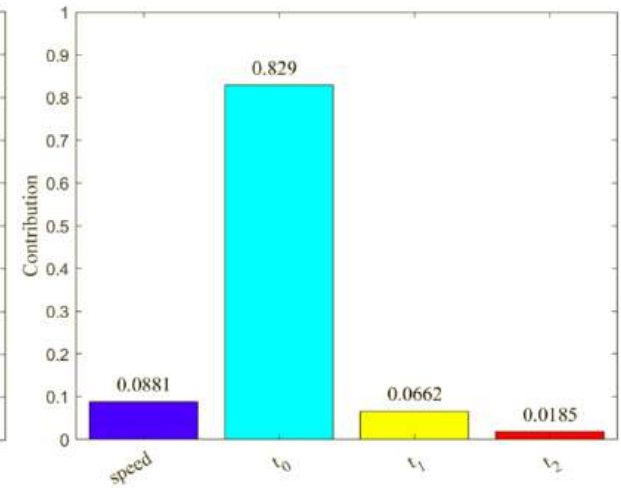
The analysis of numerical model: how input parameters are influence on the output Maximum Temperature, degree of cure and Transversal Stress



Maximum Temperature



Final degree of cure



Transversal Stresses

Laboratory of Composite Materials and Structures at Center for Design, Manufacturing, and Materials (CDMM)

- Shape distortions
- Technological defects
- Effect of process parameters
- Numerical simulation of process
- Thermoplastic pultrusion
- Process optimization



Pultrusion machine: Pultrex Px500-6T

- Pulling force: 60kN
- Pulling speed: 0.04÷5 m/min

SUMMARY

- Optimization and Surrogate Modeling in pSeven for scientific projects
- Results of application pSeven in industry oriented projects
- Design space exploration in pSeven for research – education - student projects
- Easy to connect pSeven to the numerical model in various software
- Numerical simulation of various complex problems

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